



ONERA



2nd AIAA Drag Prediction Workshop

TAU Results

O. Brodersen¹⁾, M. Rakowitz¹⁾, M. Sutcliffe²⁾

¹⁾ DLR, Institute of Aerodynamics and Flow Technology, Braunschweig, Germany

²⁾ Airbus Deutschland, Bremen, Germany



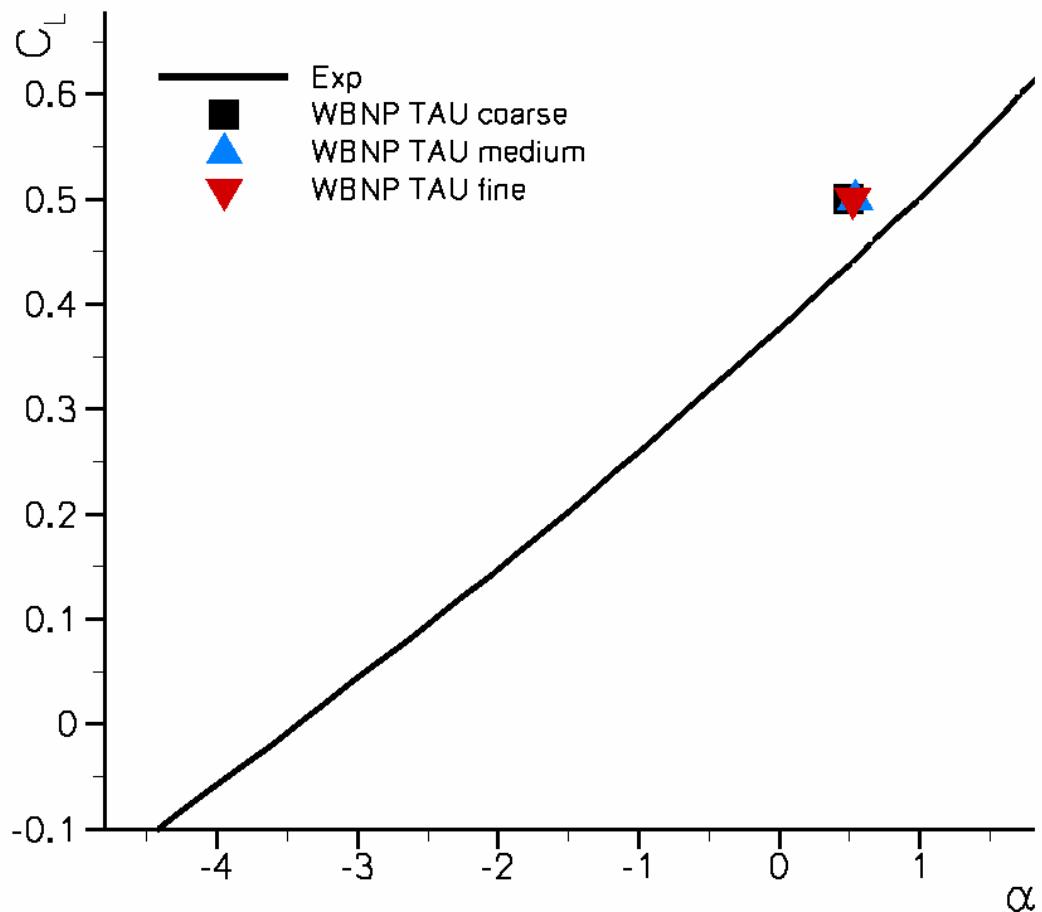
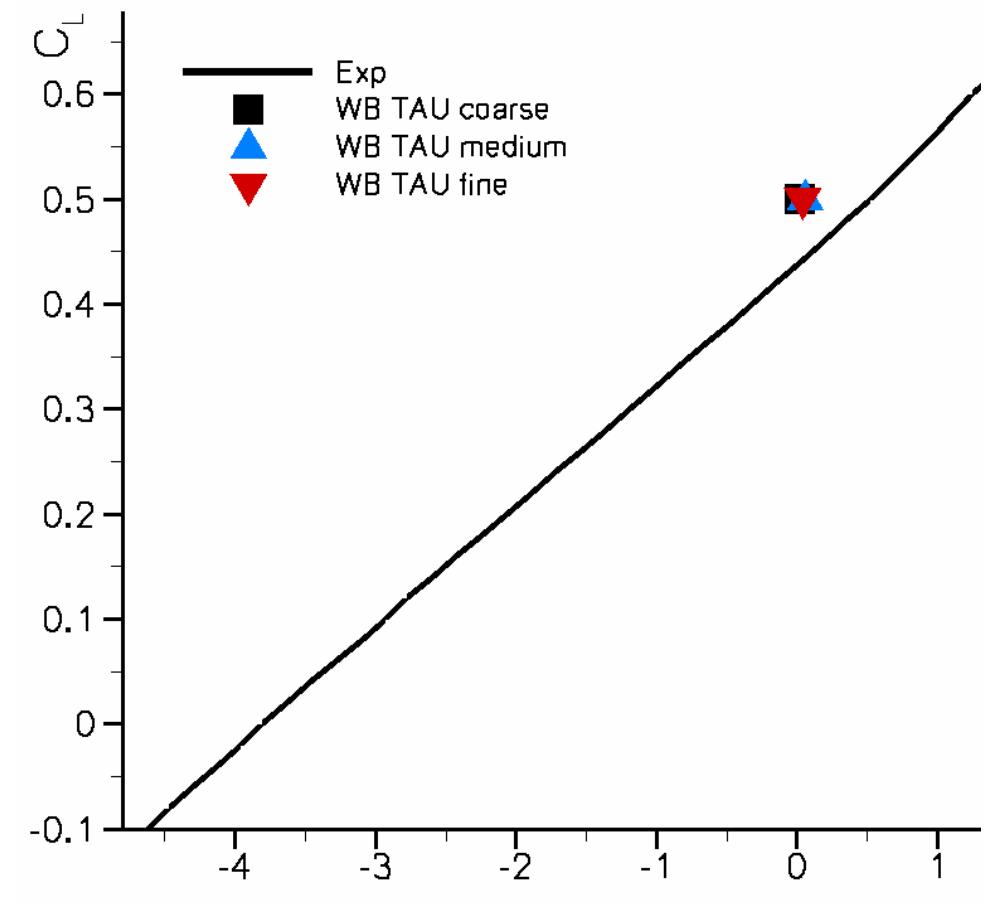
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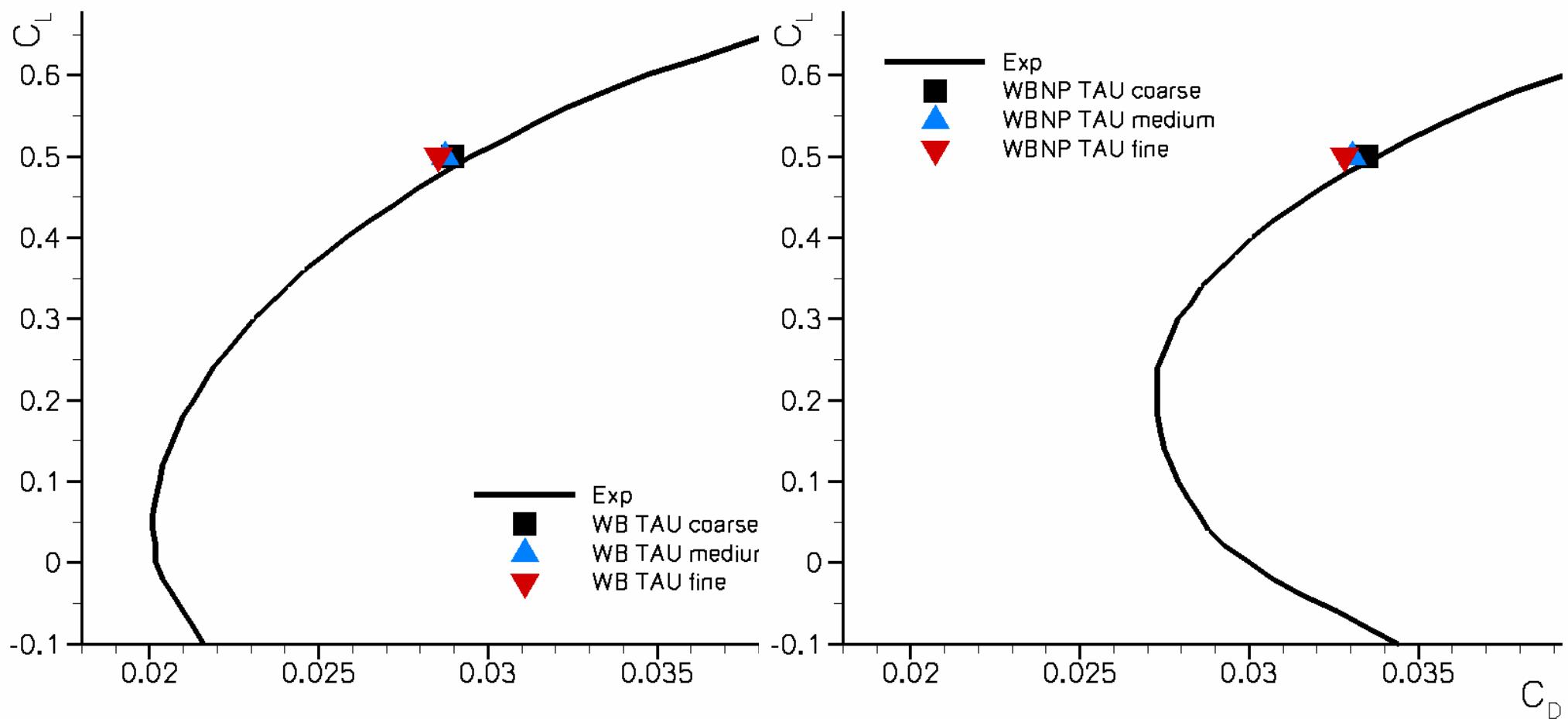
Numerical Method

- DLR-TAU software solves RANS equations
- Node-centered, hybrid grids, dual grids
- Various discretization schemes, turbulence models
- Grid adaptation
- Acceleration techniques, vectorized, parallelized
- Grids generated with Centaur from Centaursoft
- TAU was developed in the German MEGAFLOW project

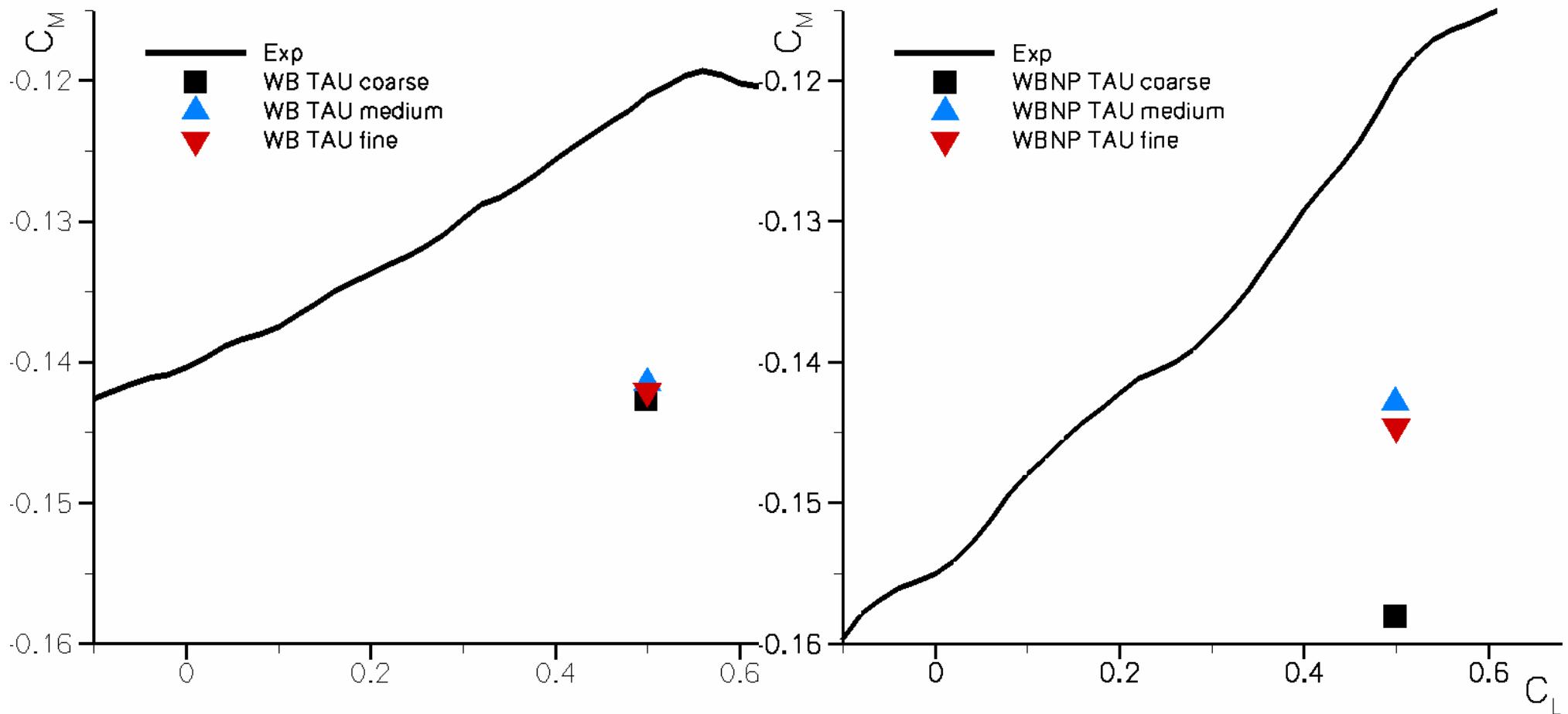
Case 1: Influence of Grid Density



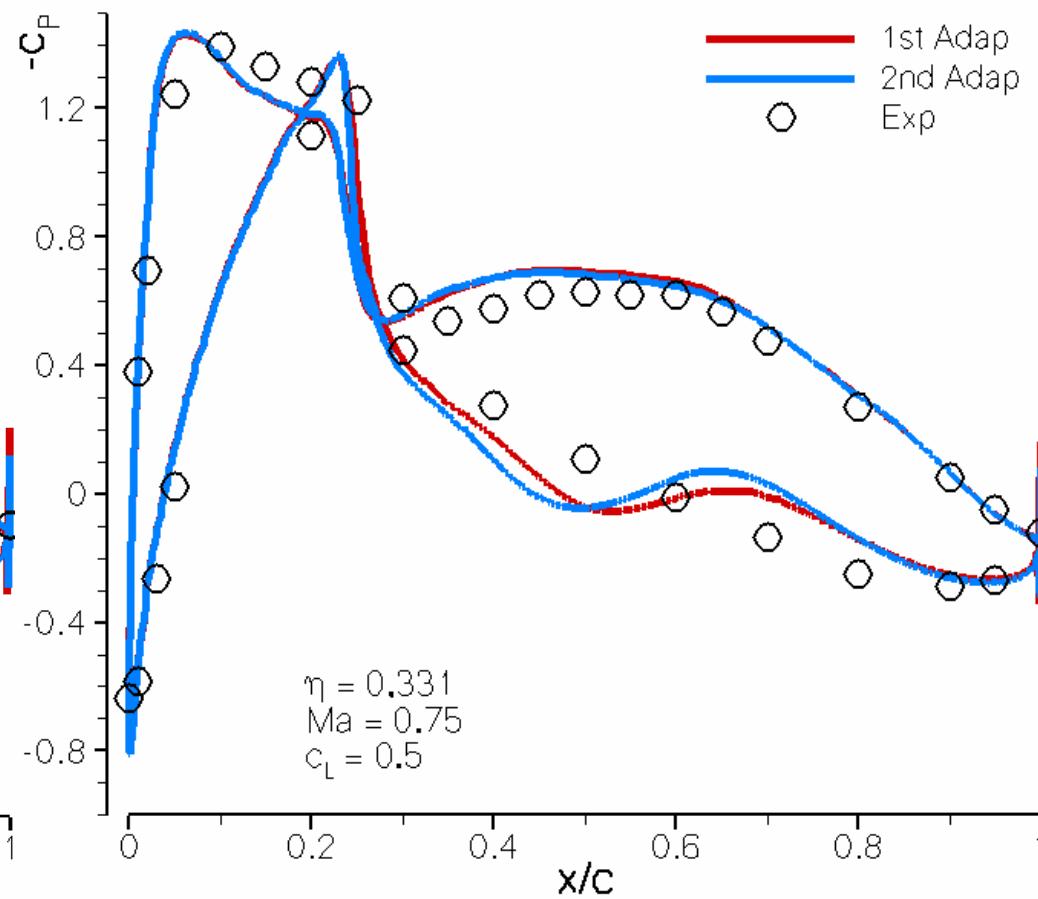
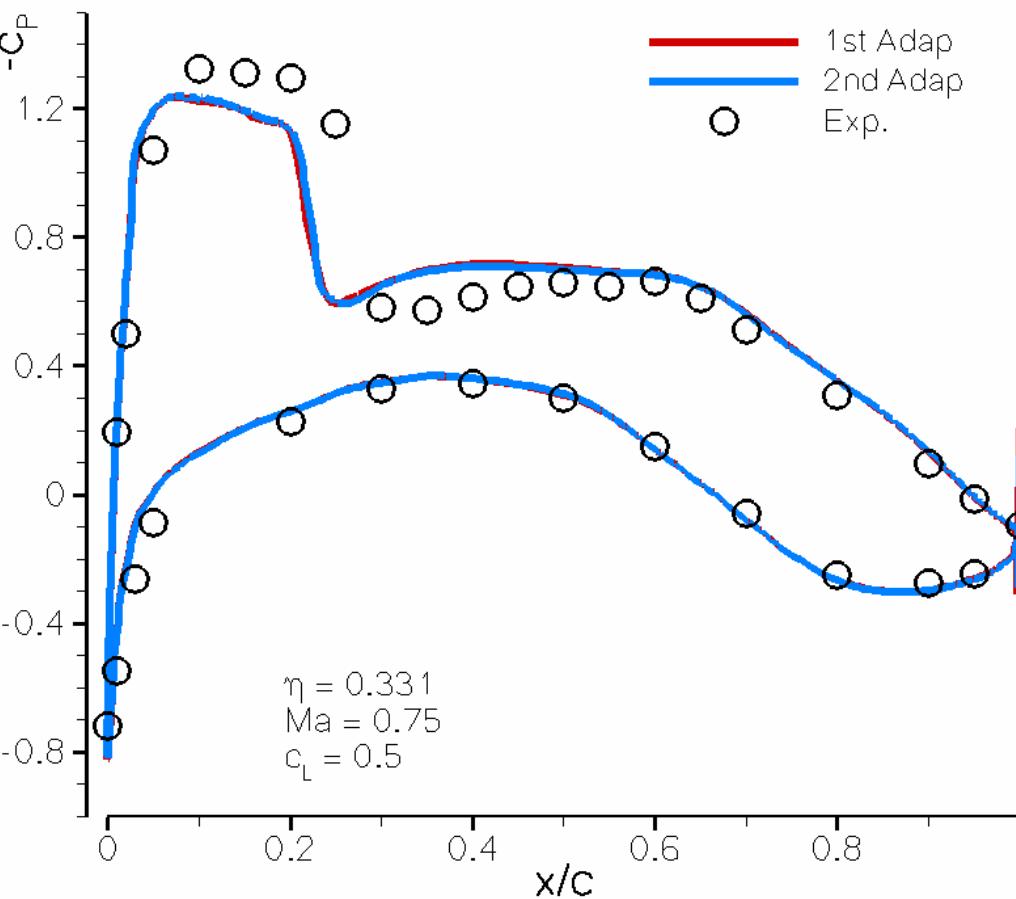
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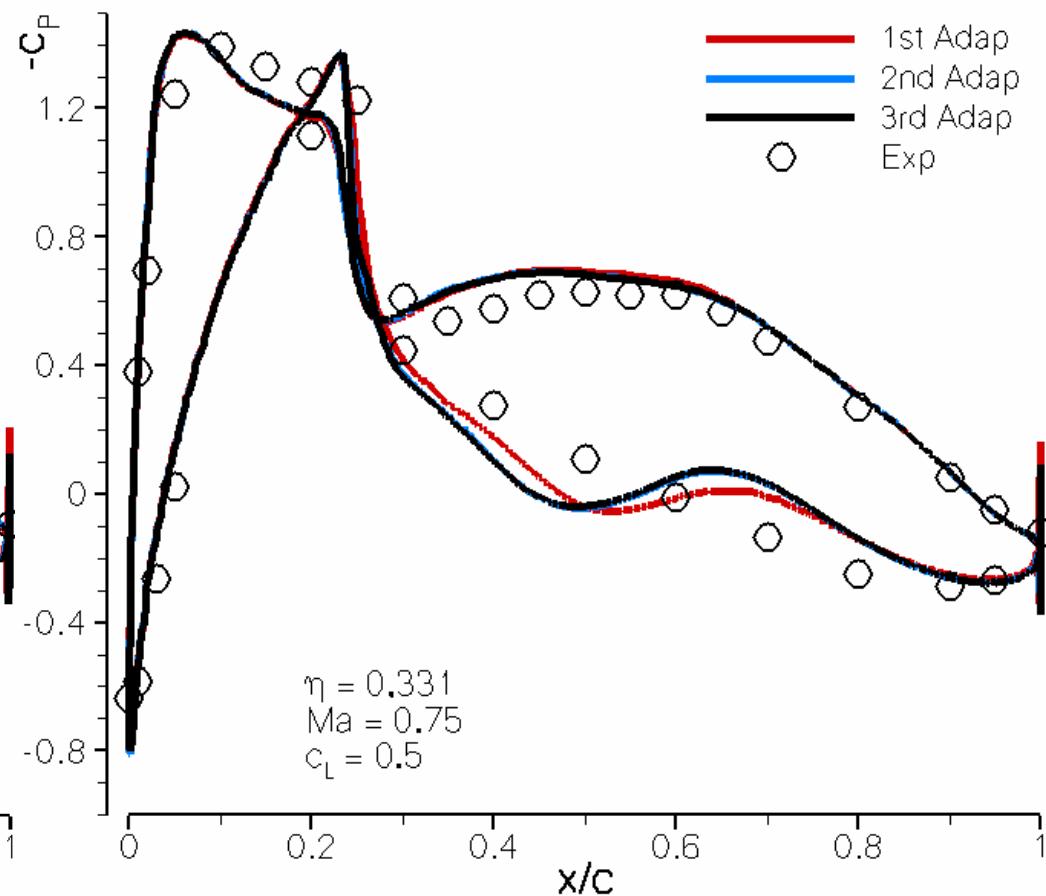
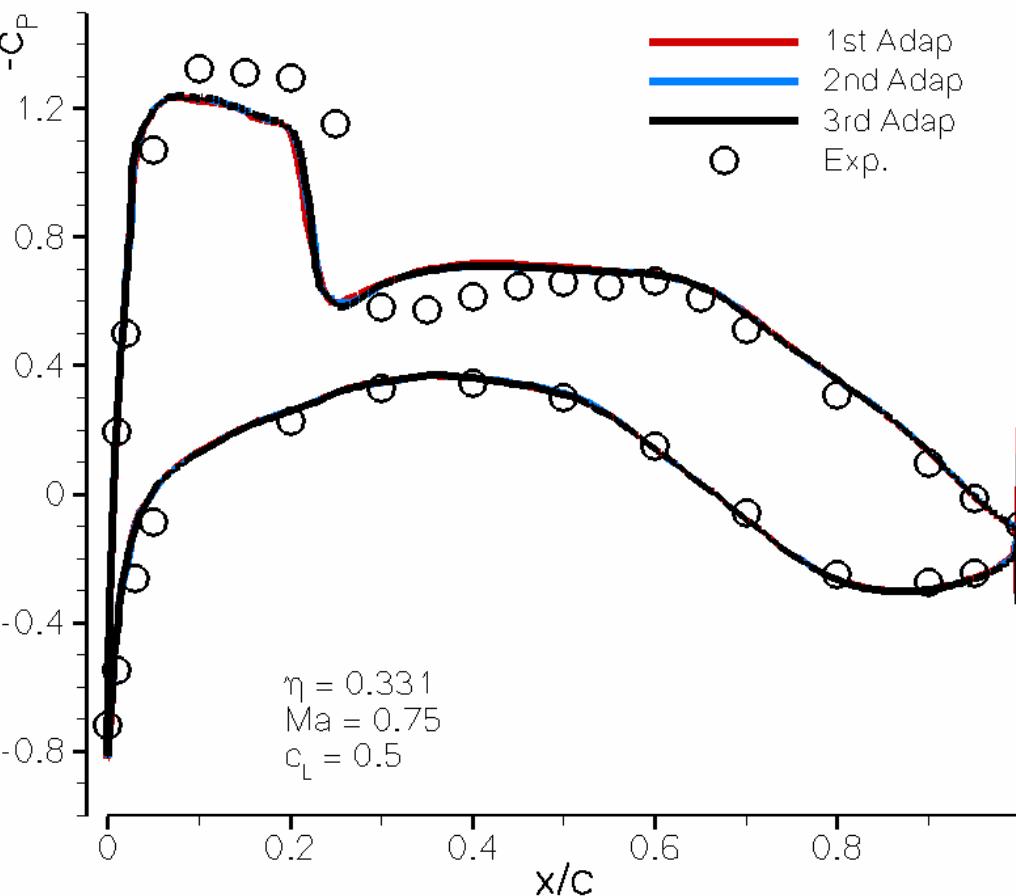
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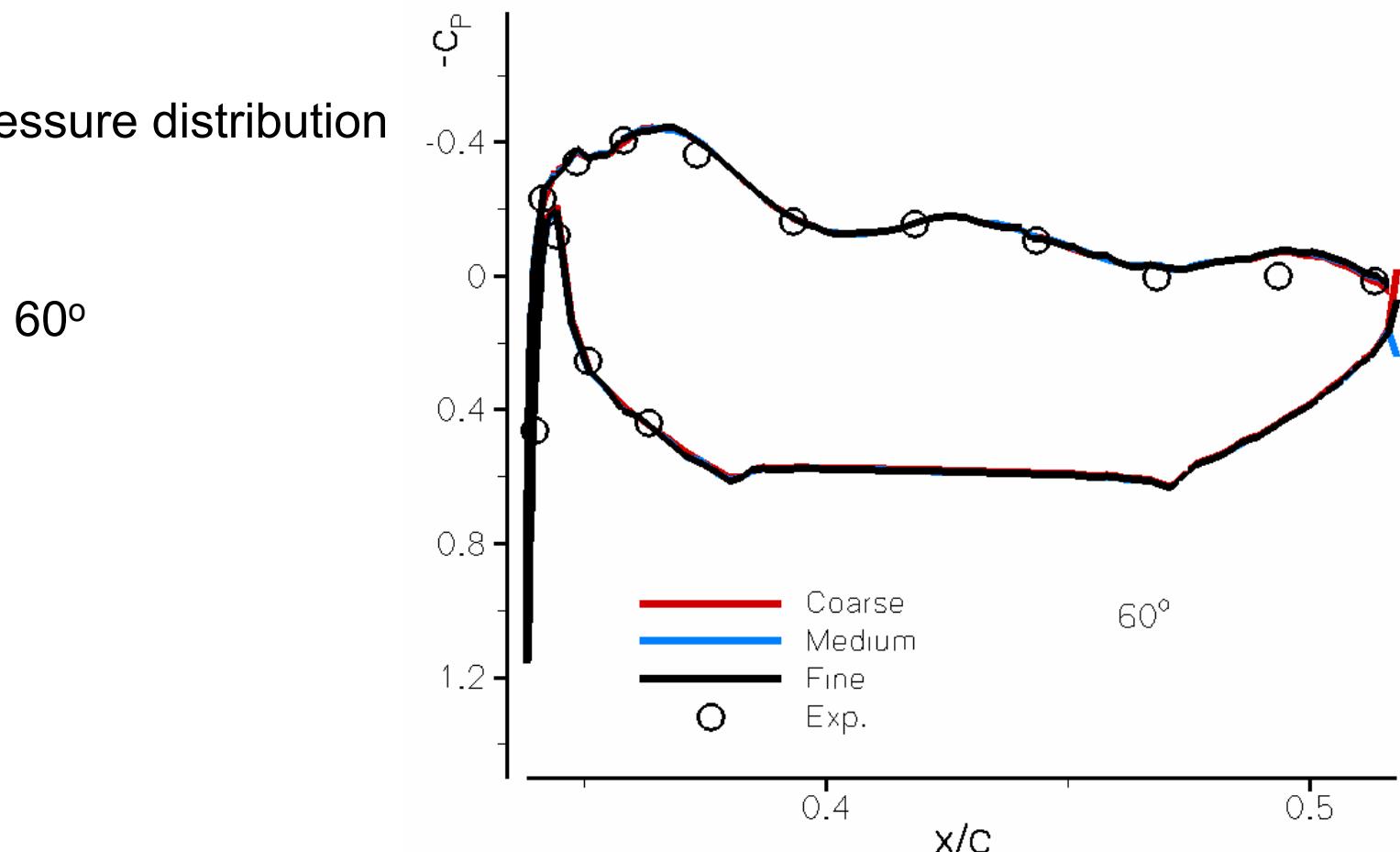


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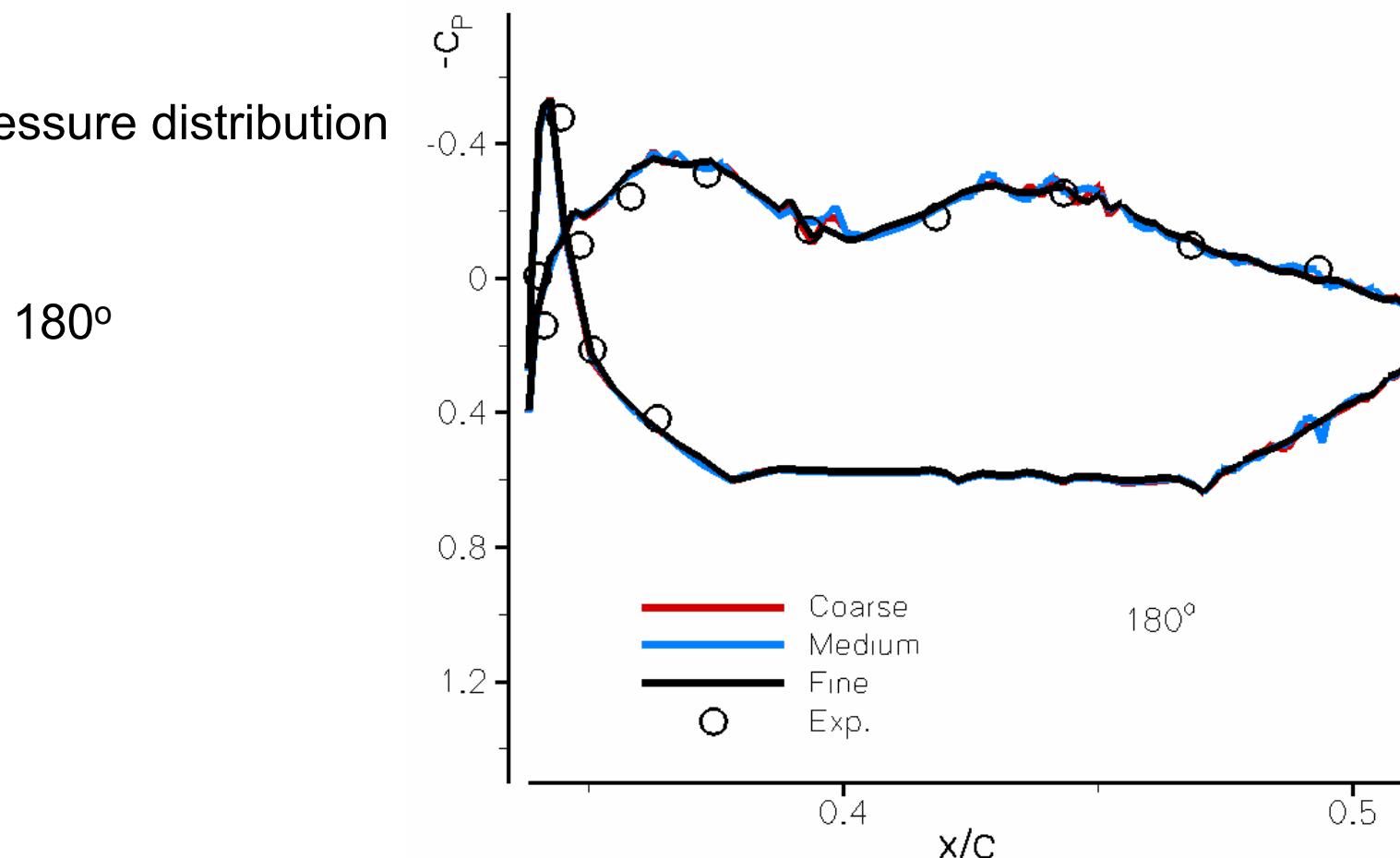
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Nacelle pressure distribution



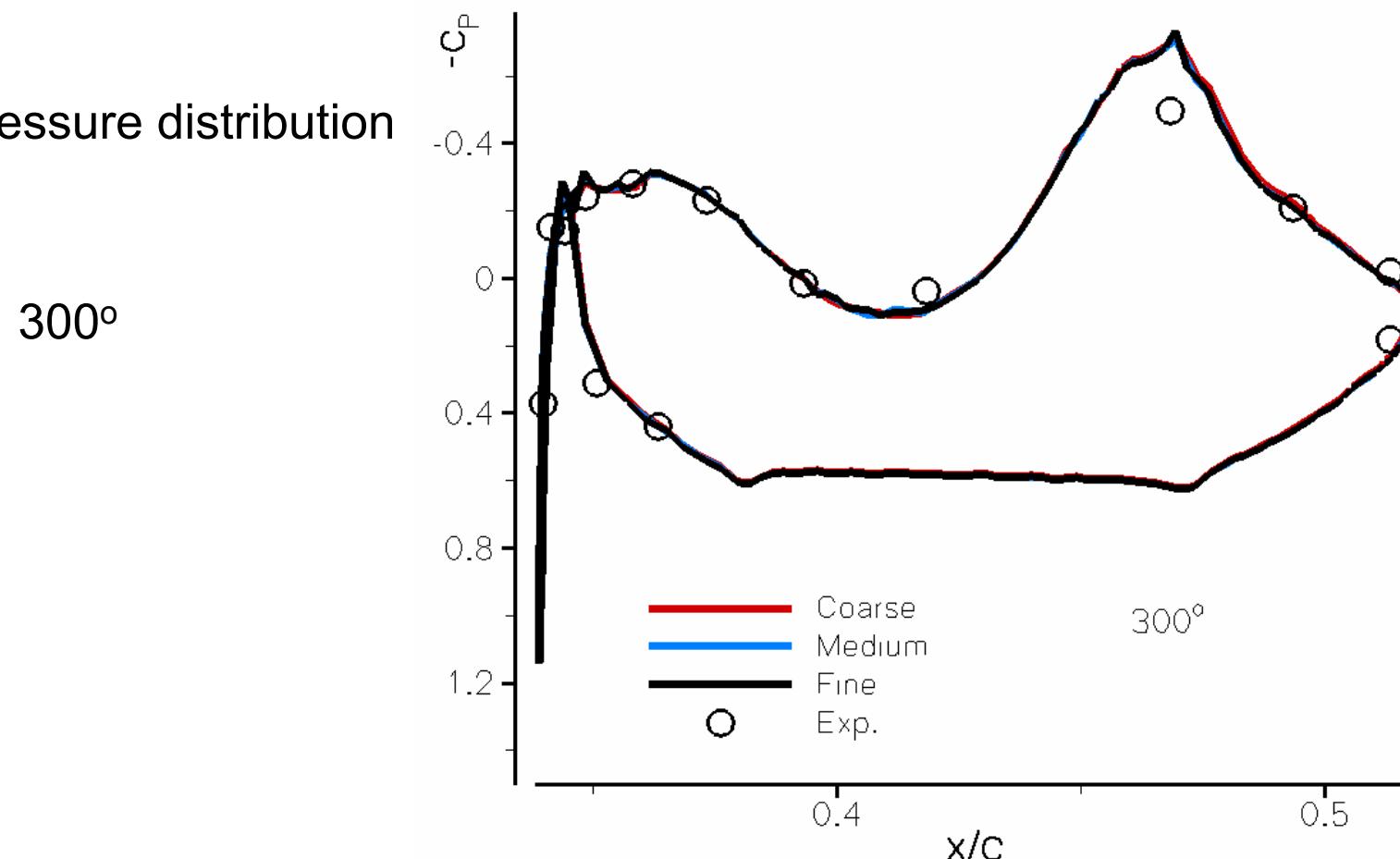
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Nacelle pressure distribution



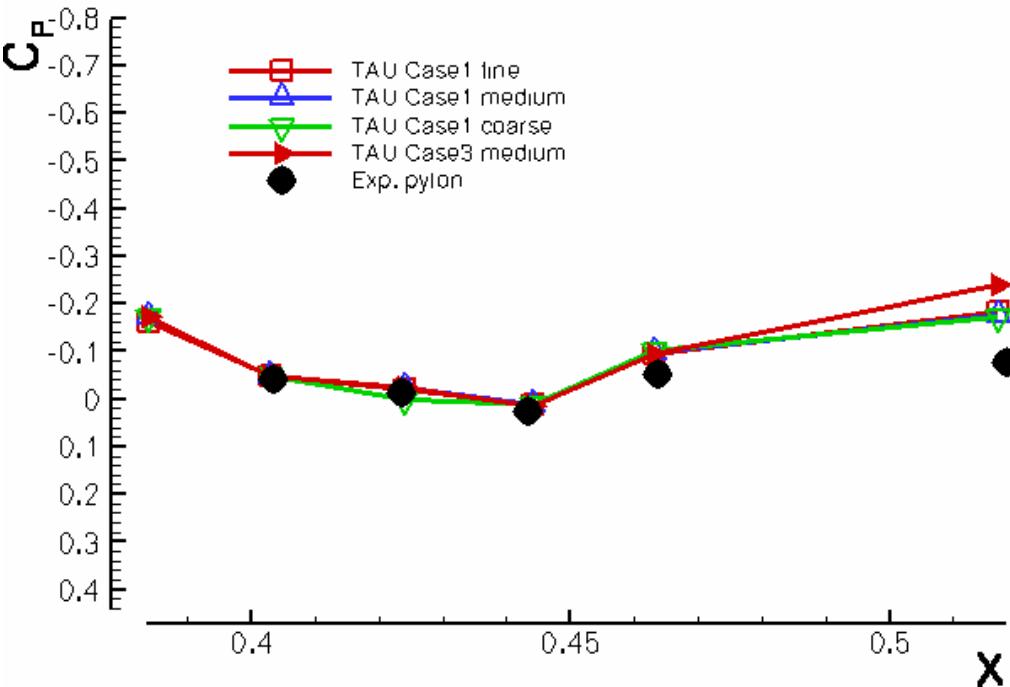
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Nacelle pressure distribution

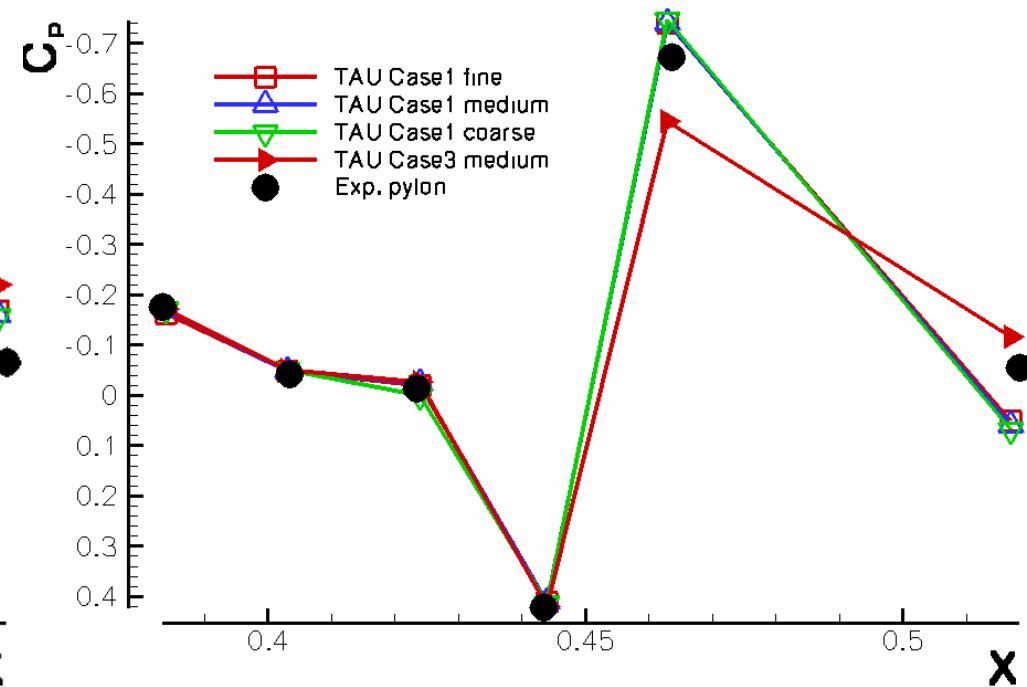


Case 1: Influence of Grid Density

F6 wbnp outboard pylon



F6 wbnp inboard pylon

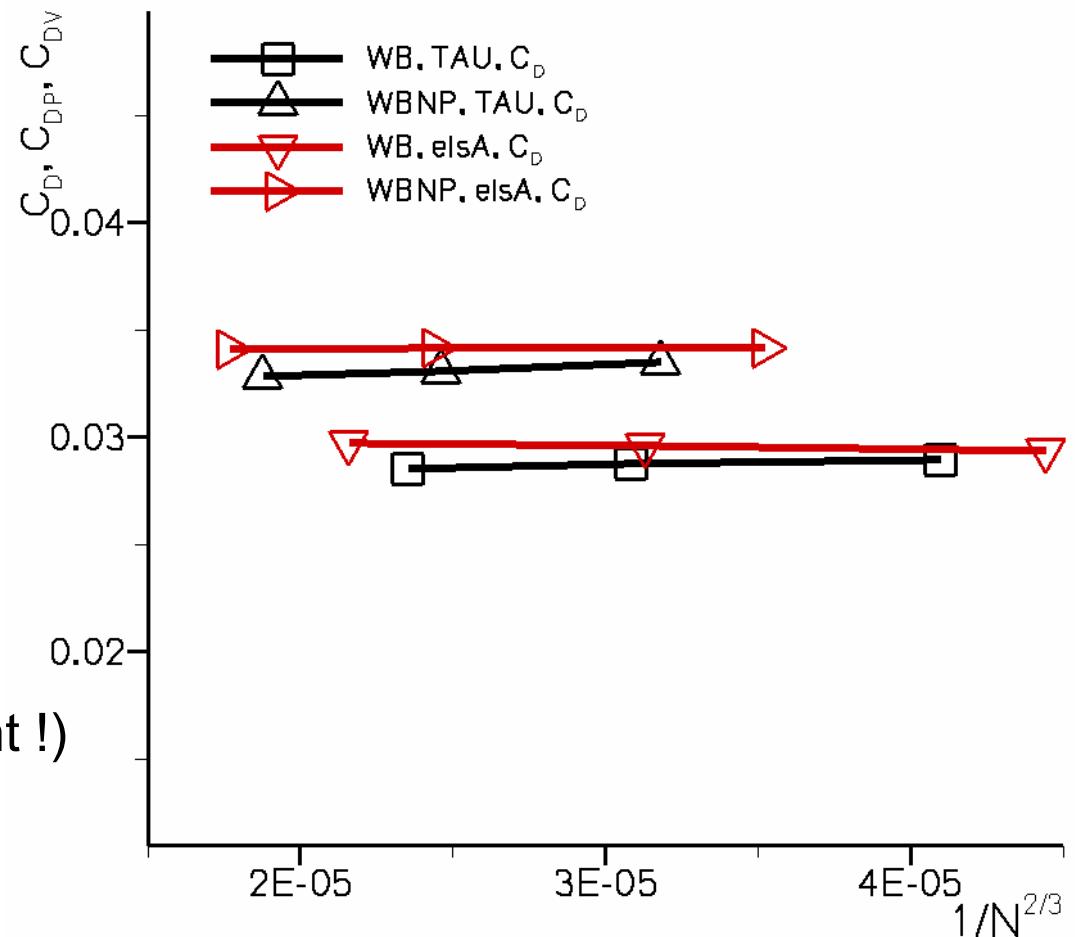


Case 1: Influence of Grid Density

ΔC_D extrapolated

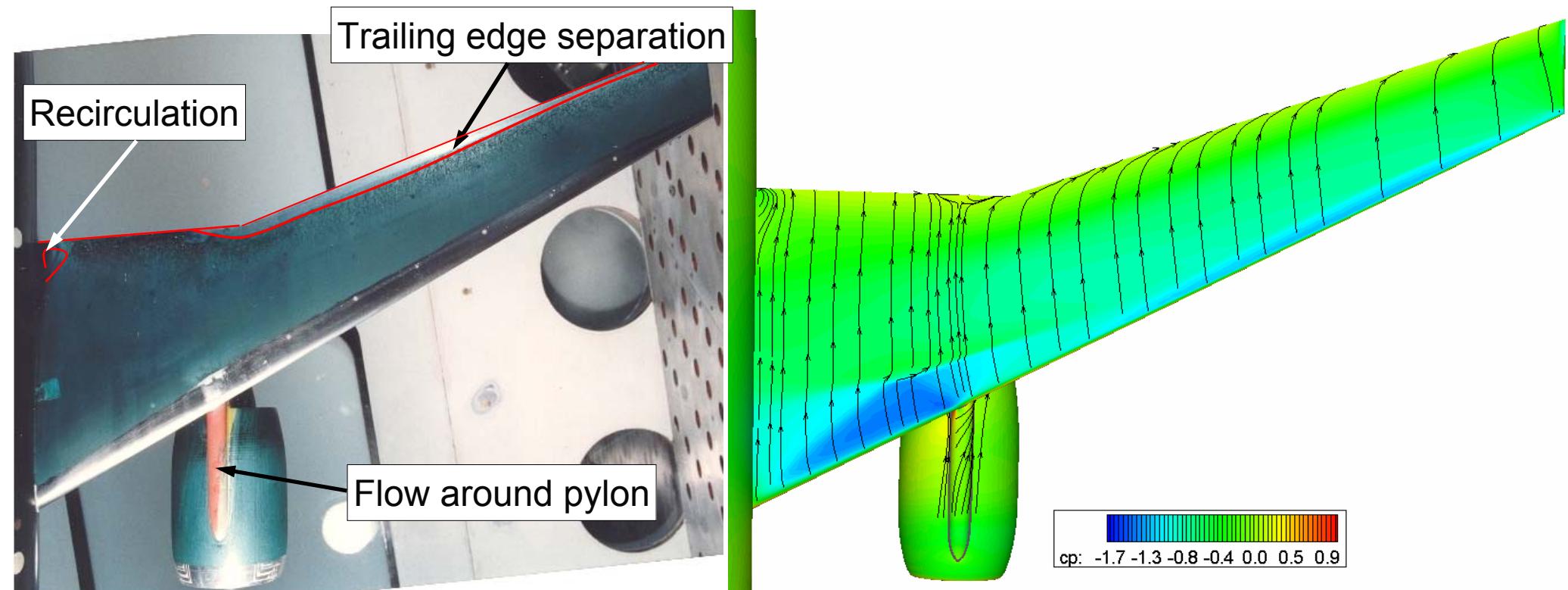
Code	WB	WBNP
TAU	-2.3%	-2.4%
elsA	+1.0%	+0.9%

elsA (ICEM grids used;
grids not suitable for grid refinement !)



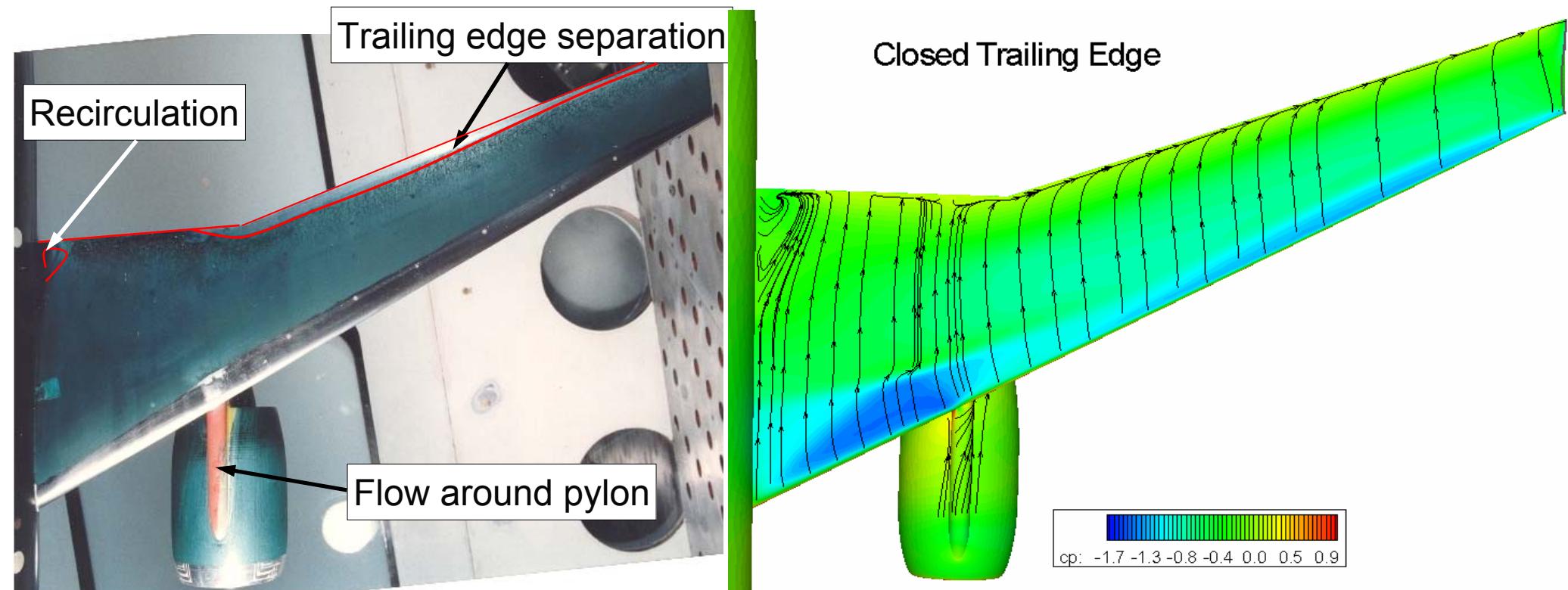
Case 1: Flow Phenomena

→ Geometry influences trailing edge separation

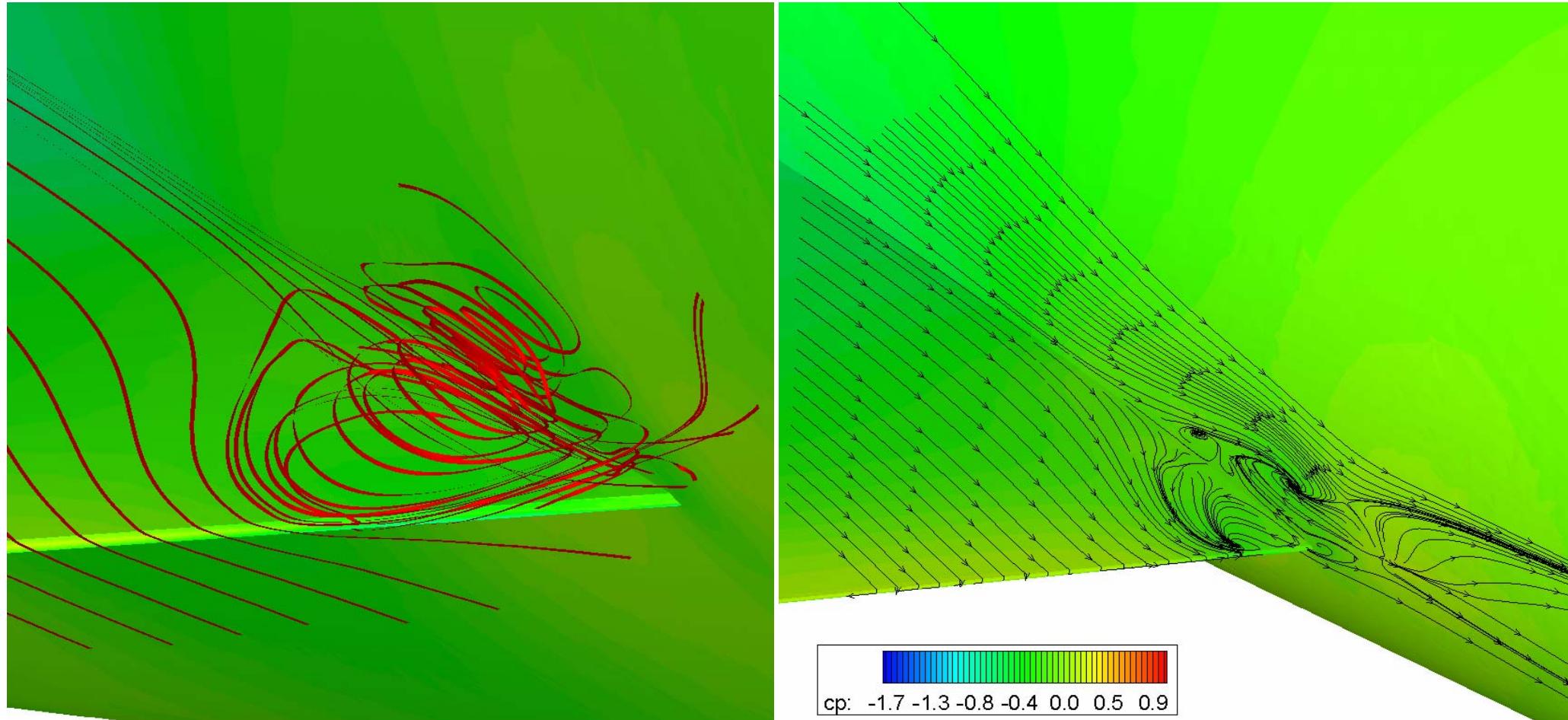


Case 1: Flow Phenomena

→ Geometry influences trailing edge separation

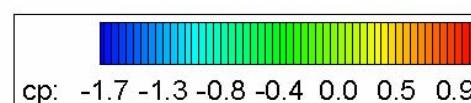
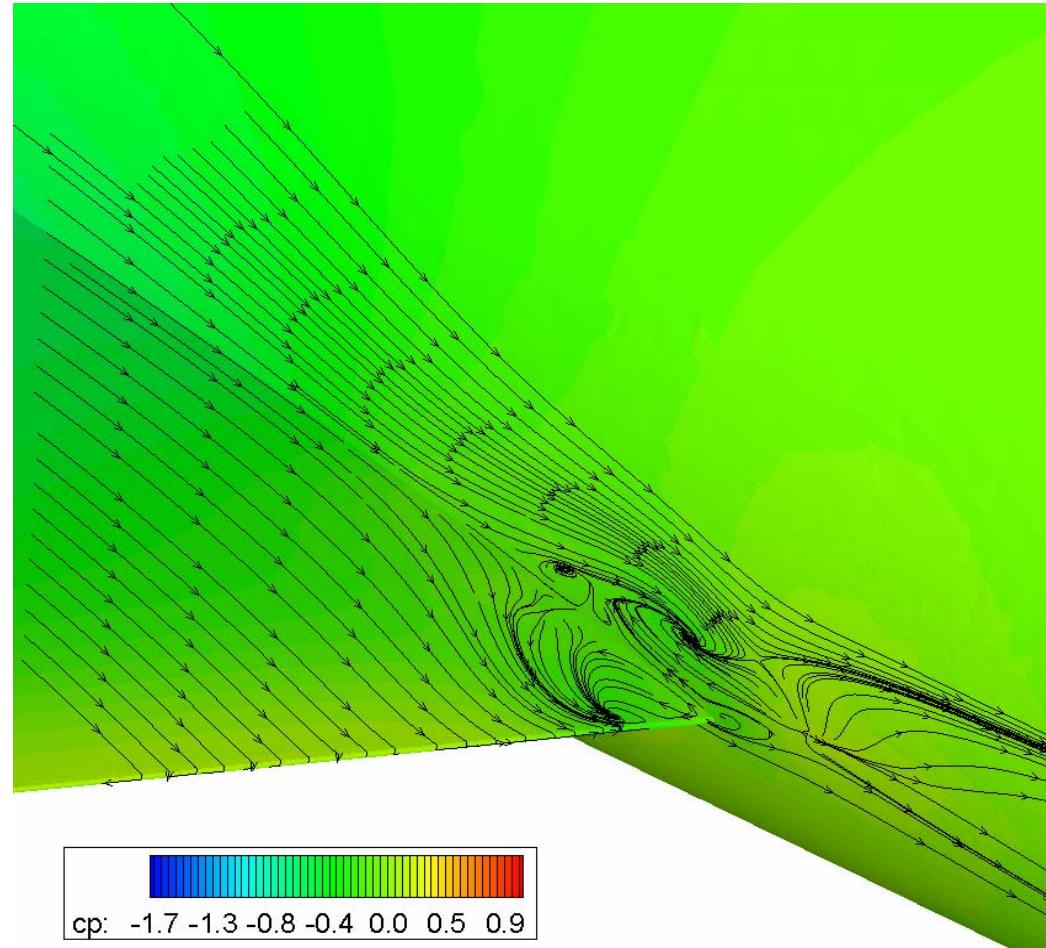


Case 1: Flow Phenomena

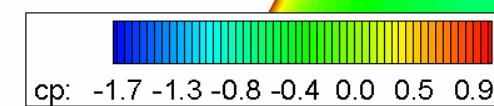
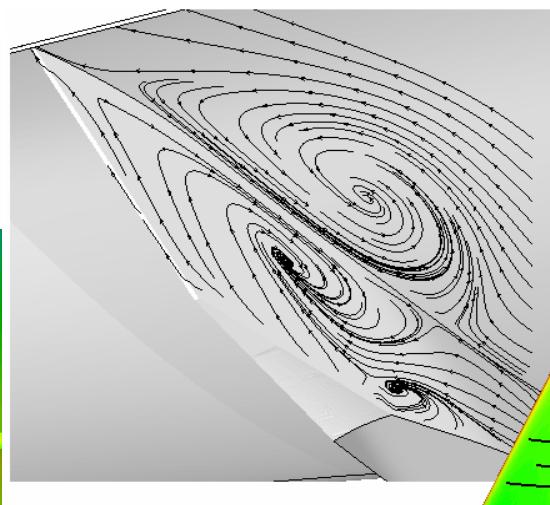
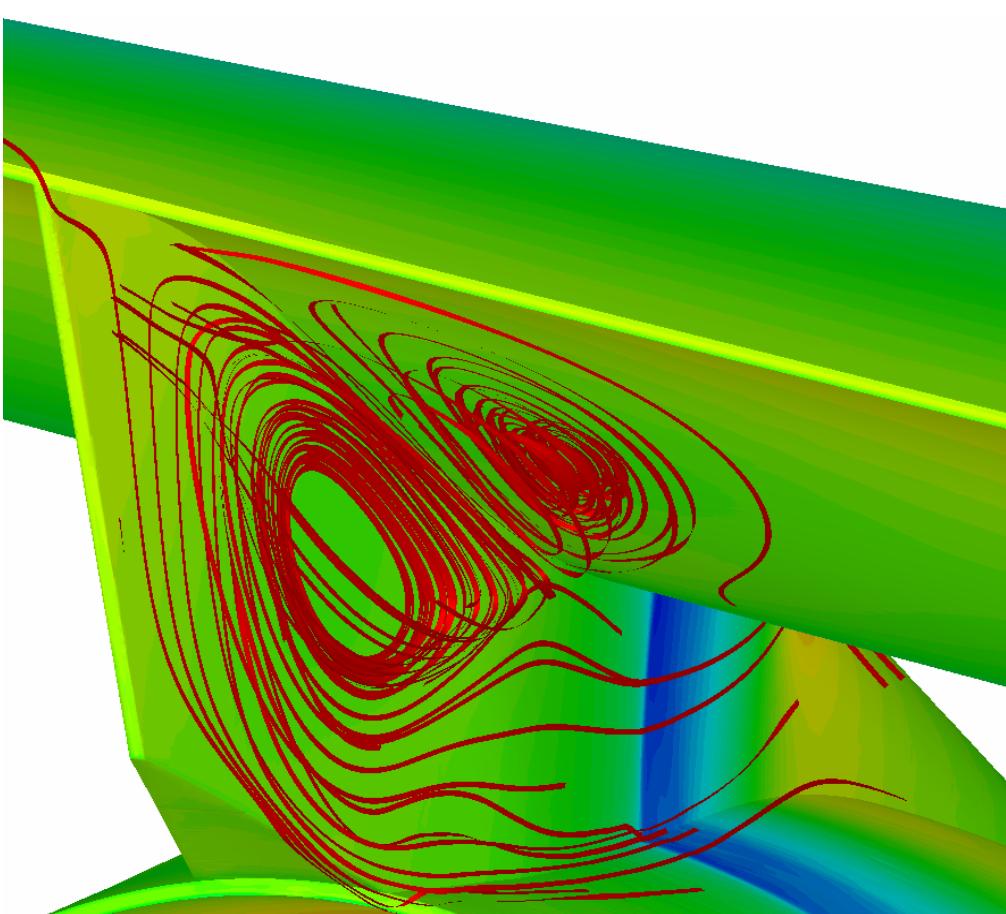


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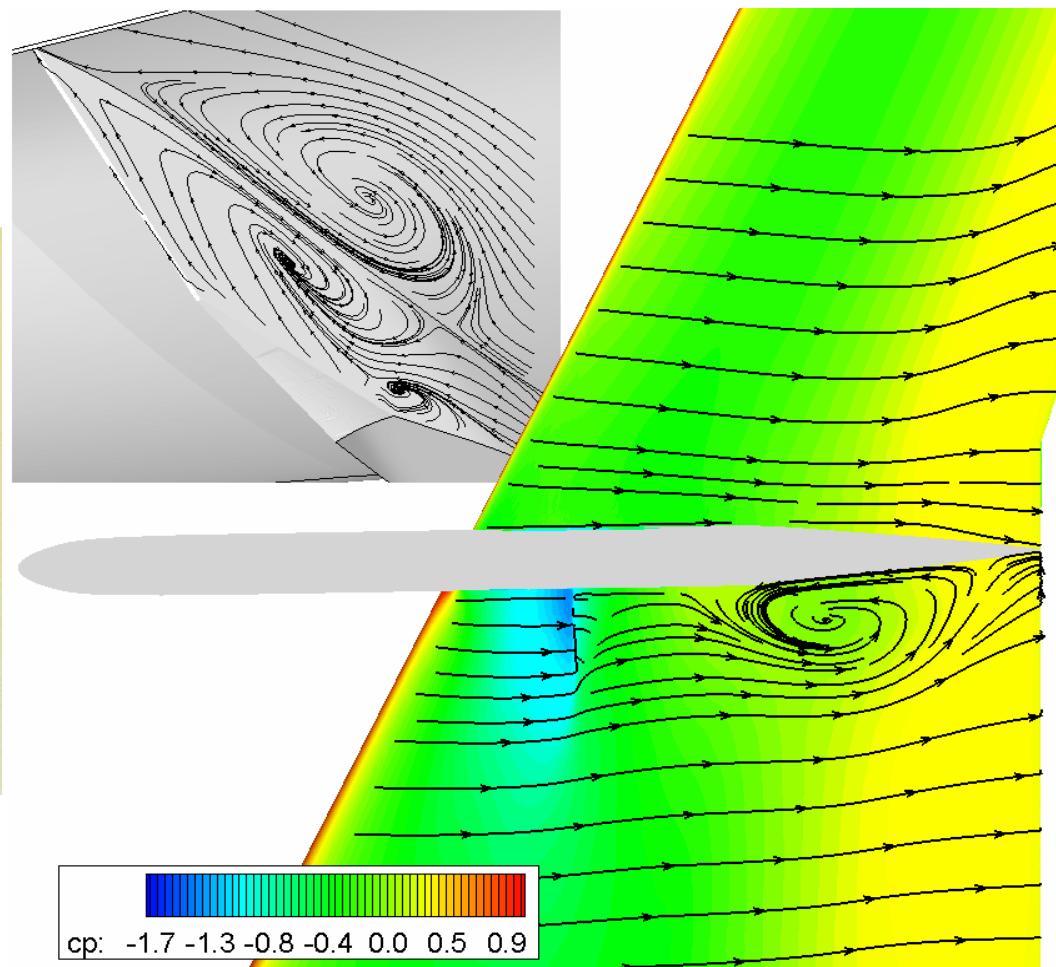
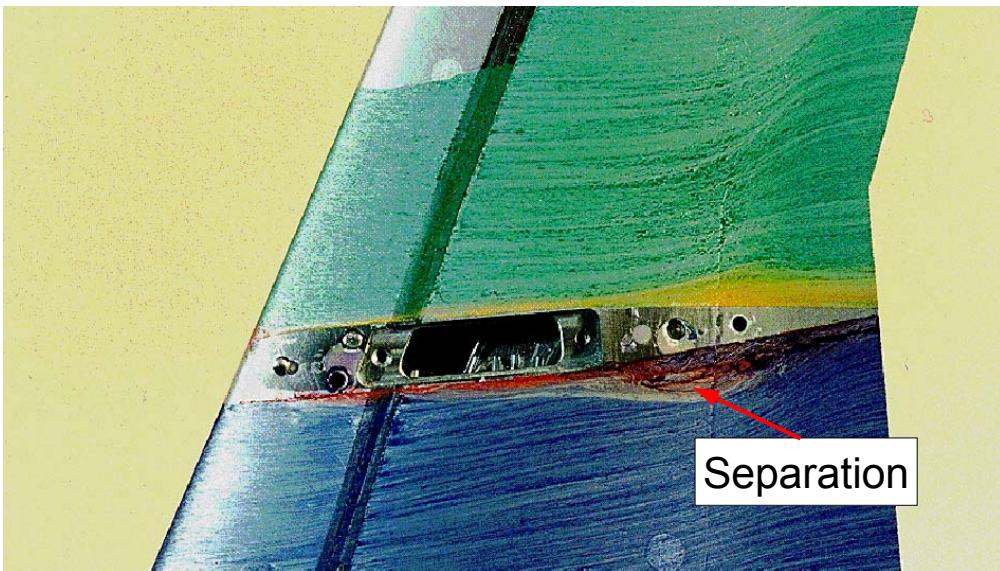
Separation



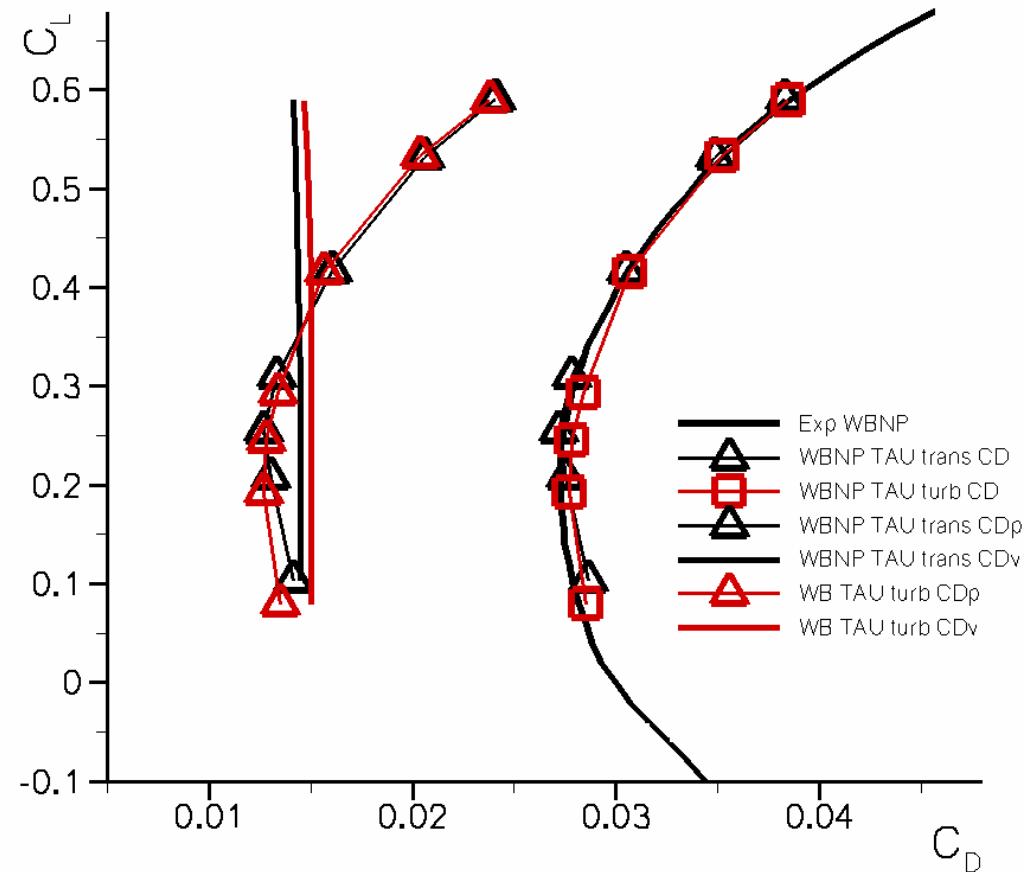
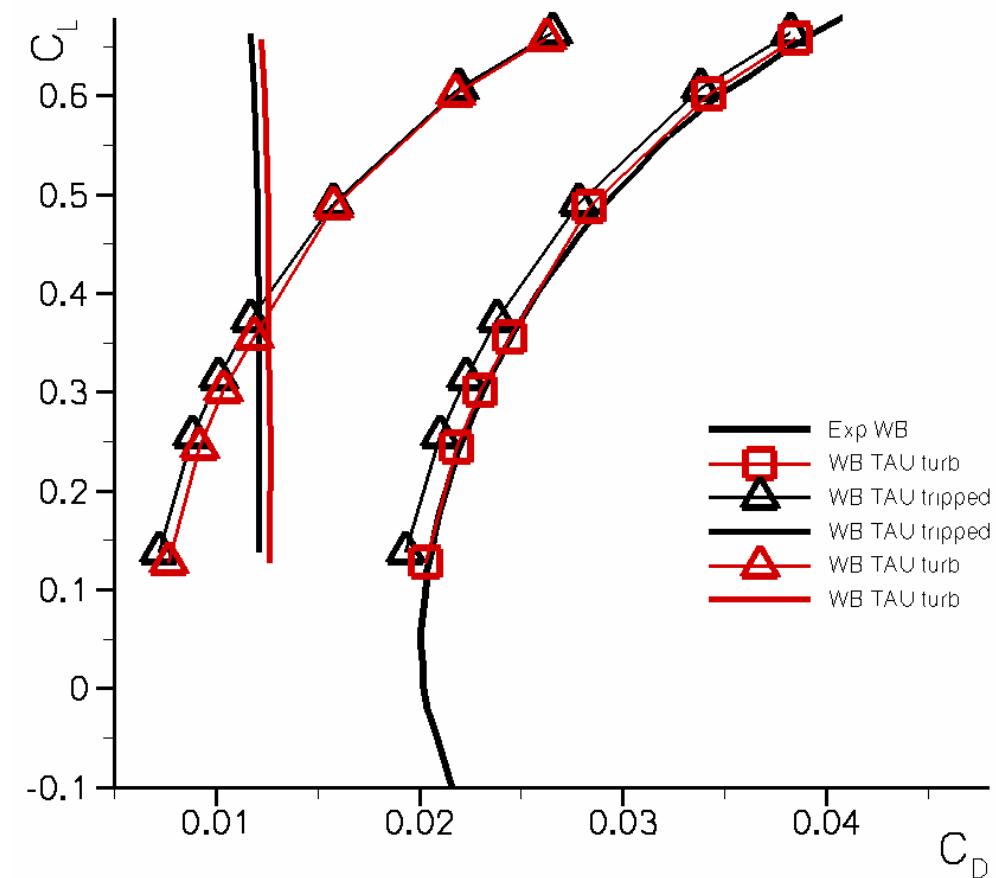
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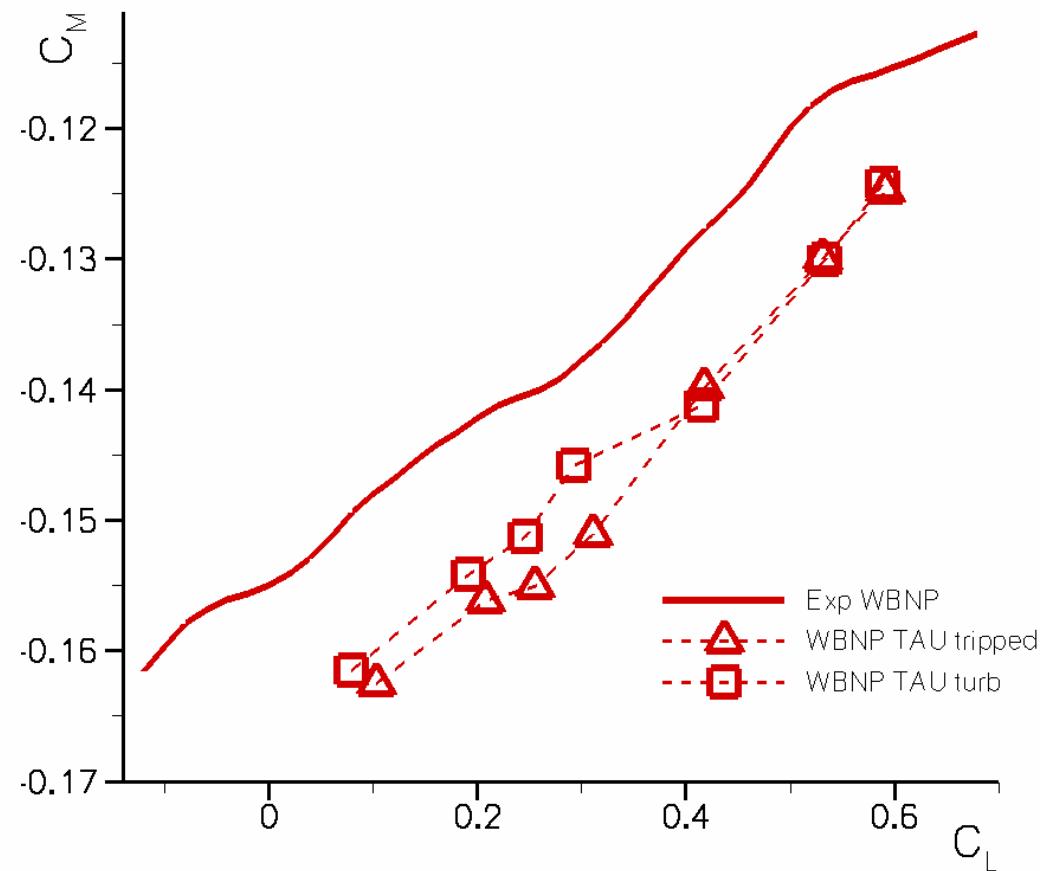
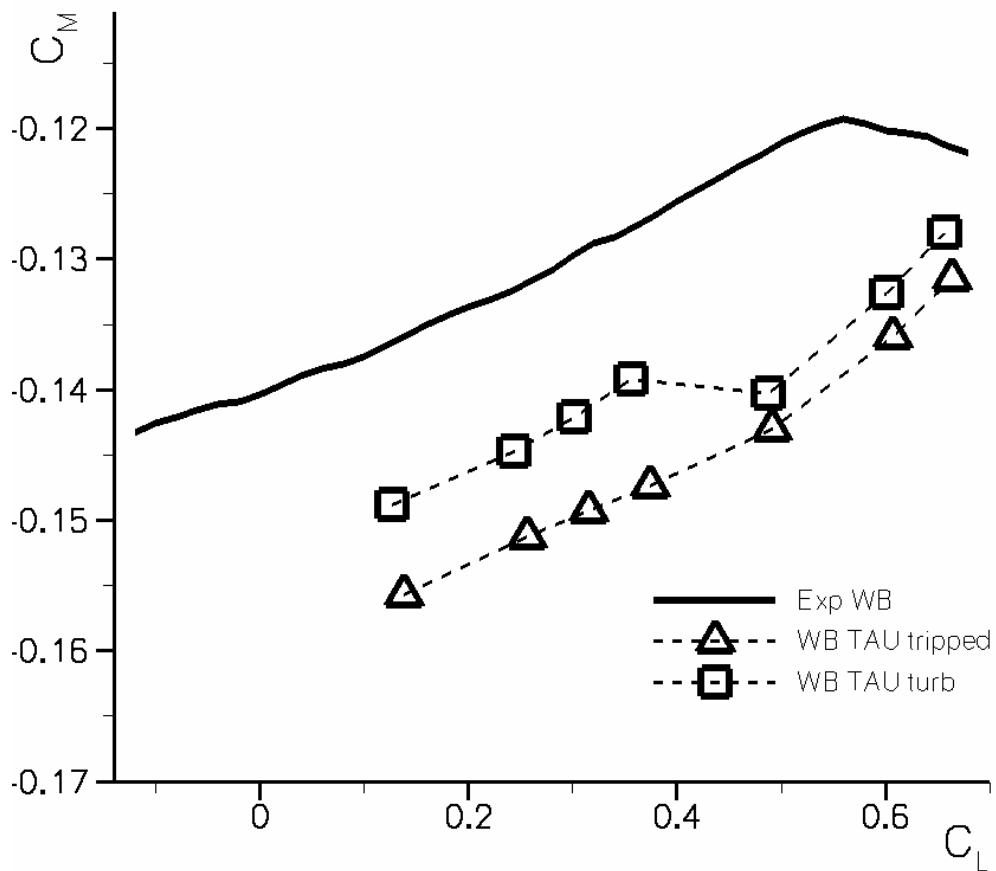
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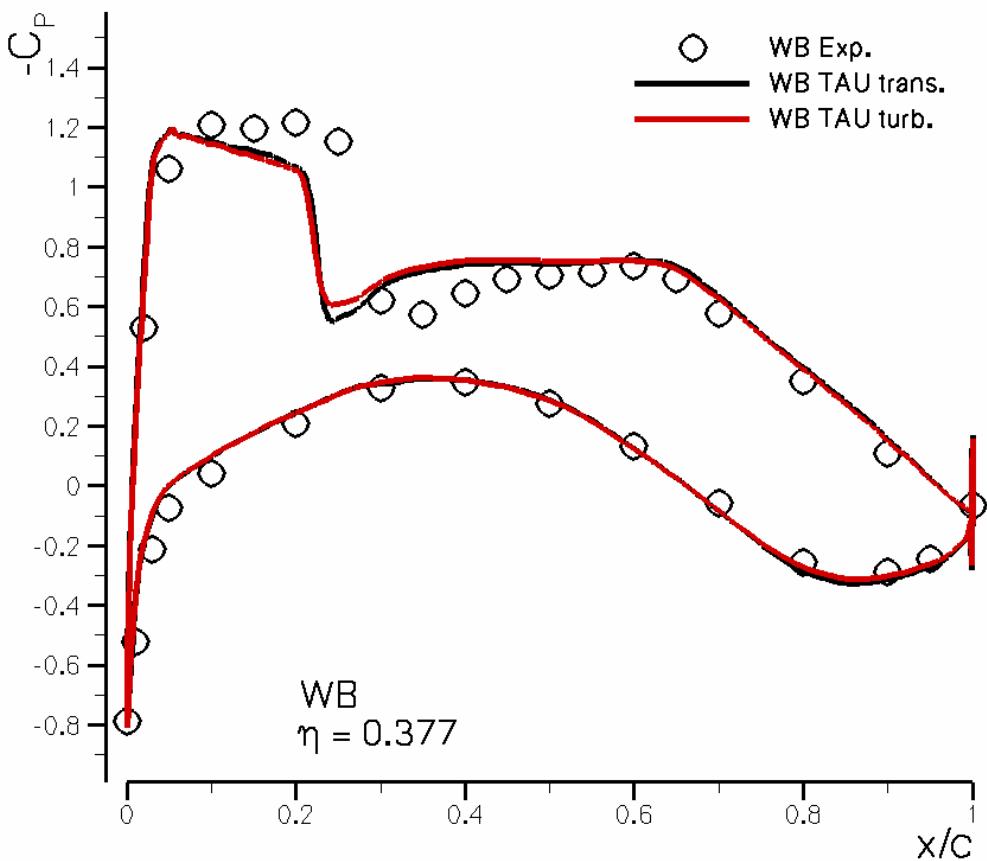
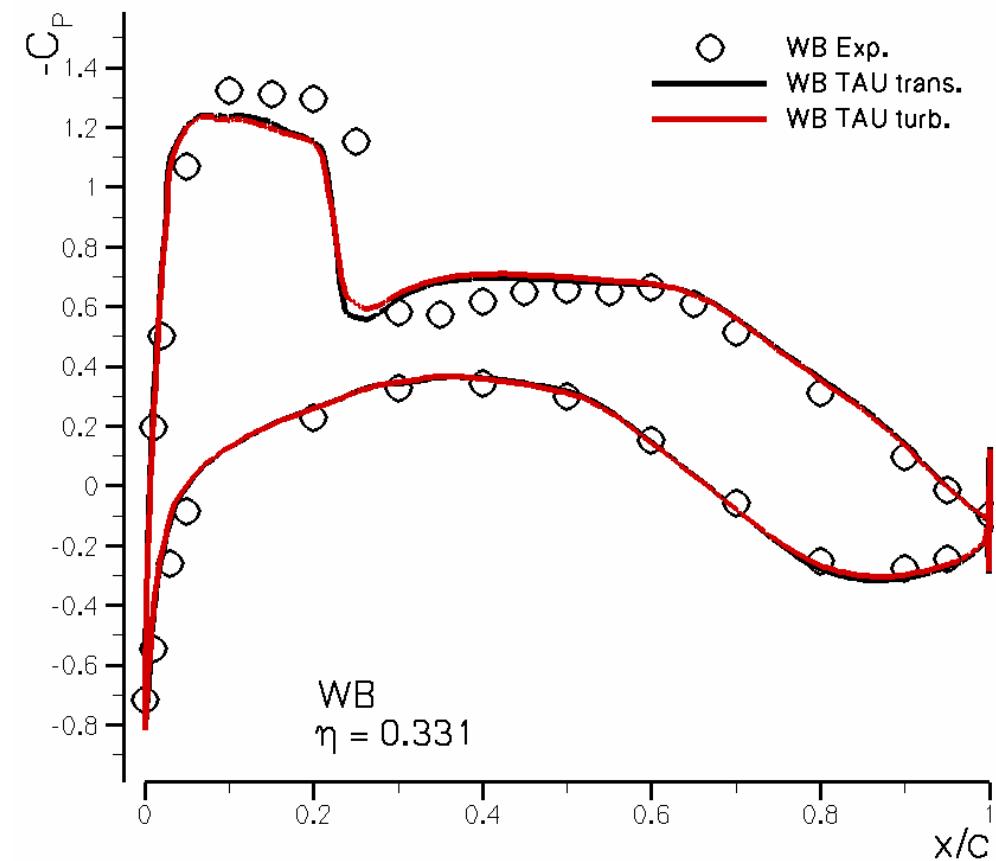
Case 2: Drag Coefficients



Case 2: Moment Coefficients

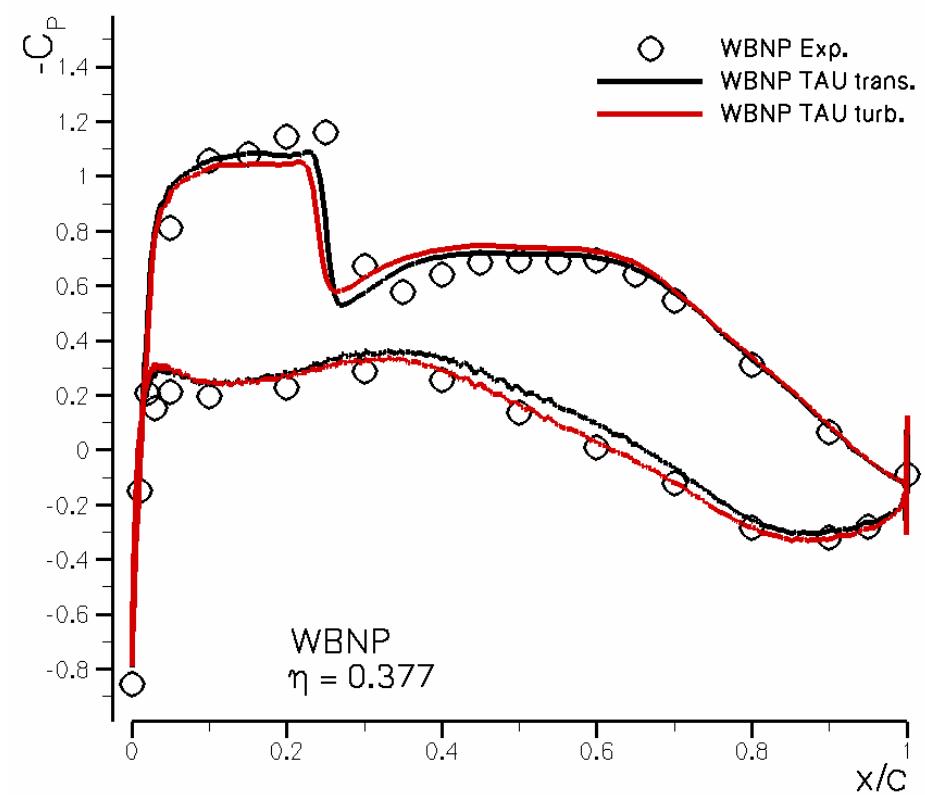


Case 3: Comparison with transition / fully turbulent



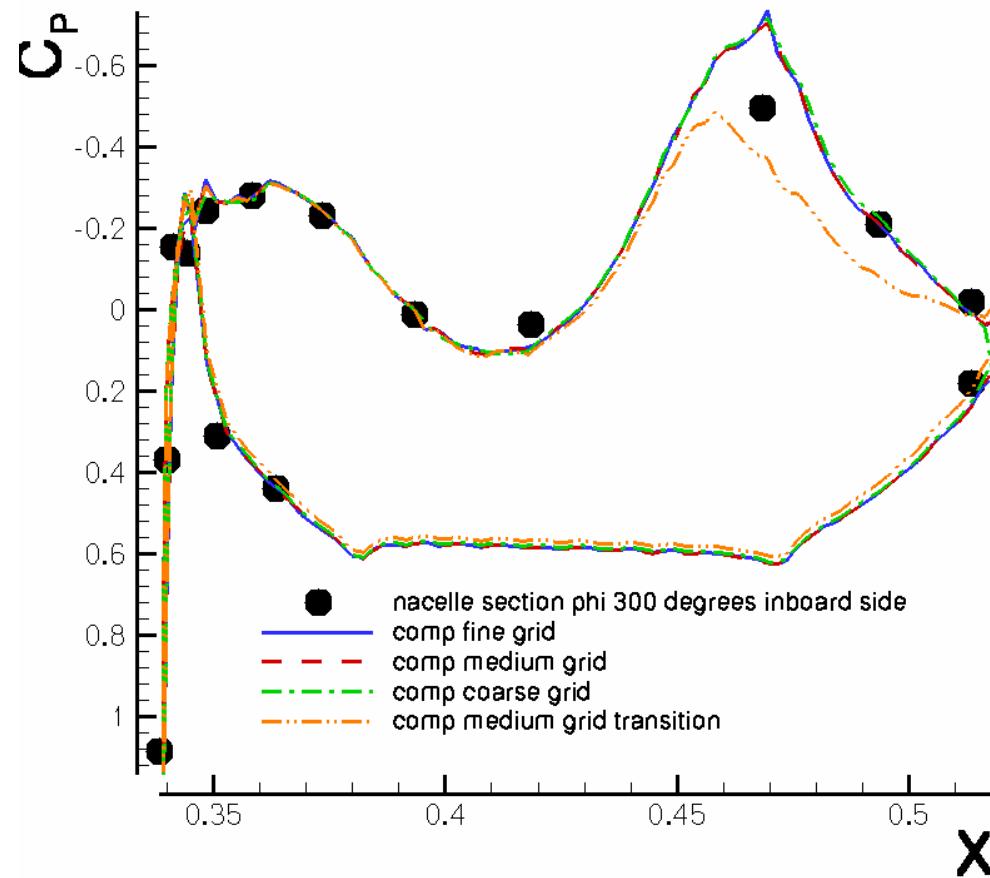
Case 3: Comparison with transition / fully turbulent

Conf.	C_D Trans.	C_D Turb.	ΔC_D
WB	287.4	282.1	5.3
WBNP	330.6	329.0	1.6

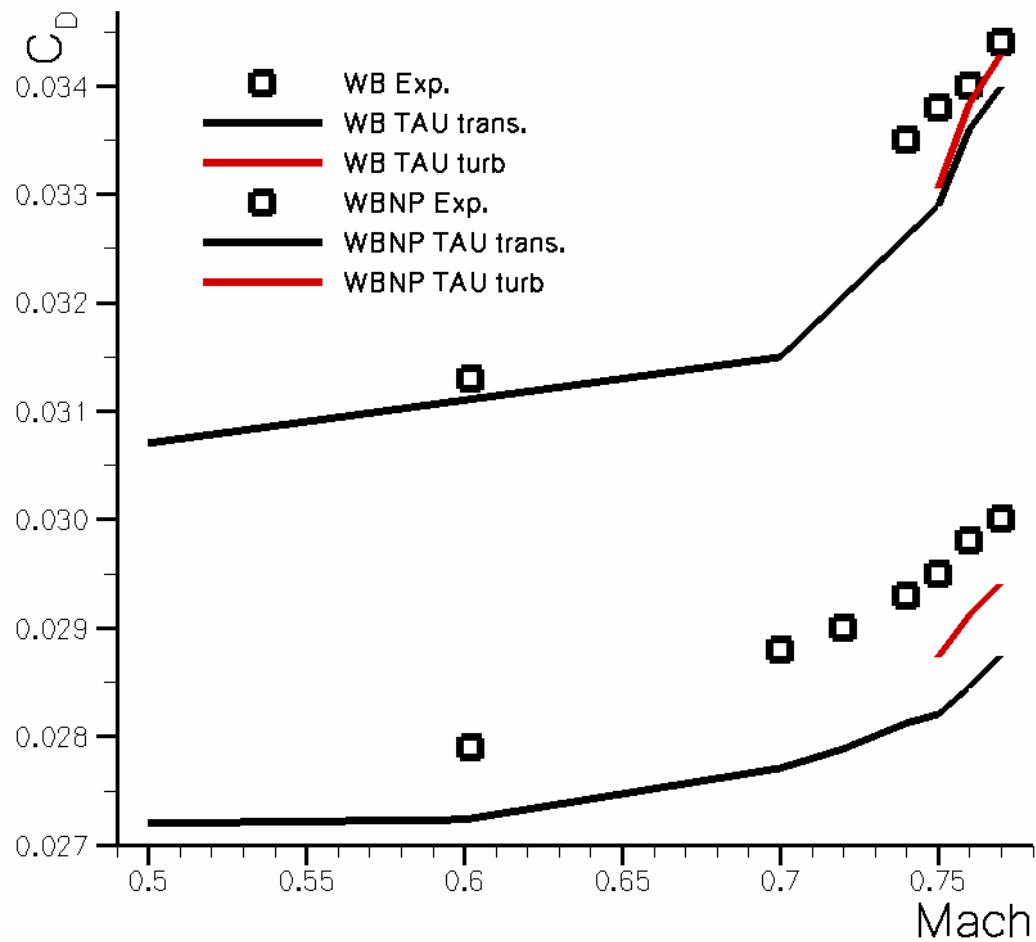


Case 3: Comparison with transition / fully turbulent

F6 wbnp nacelle 300 deg cut



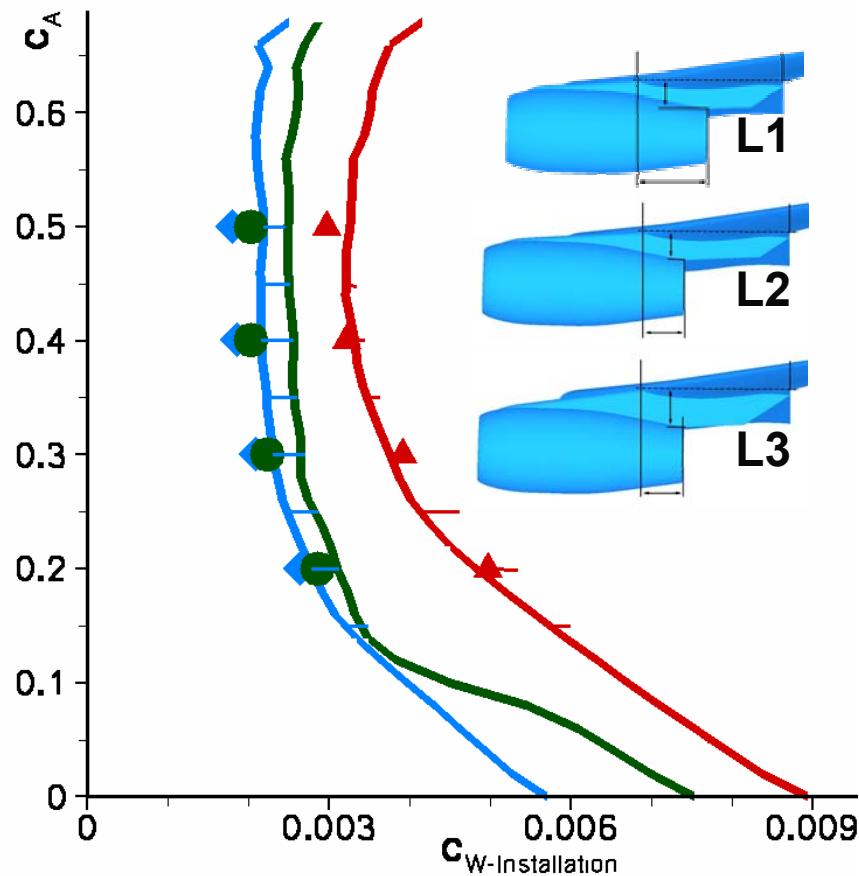
Case 4: Mach Drag Rise



DLR-F6 Cases: Installation drag

(AIAA-Journal Vol. 39, No. 6, Nov-Dec 2002)

$C_{D-Install.}$	Exp.	TAU
L1 – L2	10.7	11.8
L2 – L3	3.0	2.3



Summary

- Hybrid method (TAU & Centaur) is able to predict drag for DLR-F6 within a range of 5-8% ($C_L=0.5$)
- Grid adaptations are necessary to reduce discretization errors
- Flow phenomena have to be computed correctly to ensure drag prediction
- Trailing edge geometry of DLR-F6 has an influence on wing upper side flow separations
- Wing lower side transition is of importance
- Drag differences of 1-2 dc can be computed when errors are systematic
- Remaining questions: transition, trailing edge effects